

# Lecture - 7

13-04-2020

MicroWave Engg.

EC - 6<sup>th</sup> Sem (3<sup>rd</sup> yr.)

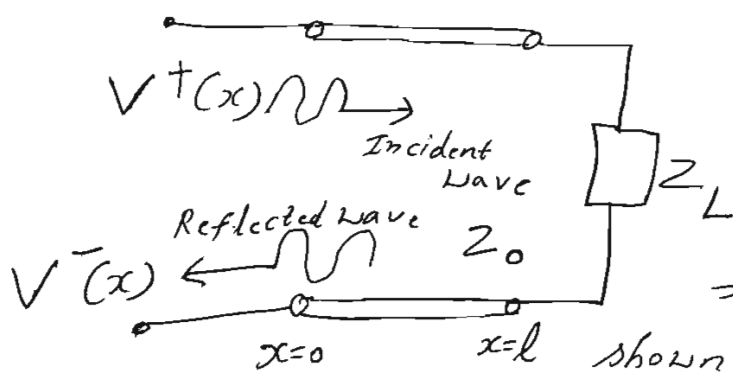
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## Relation b/w S-Parameters & ABCD Parameters

Step-1 Define waves in terms of voltages & currents

⇒ Let's take a simple transmission line, which has been terminated with a load impedance  $Z_L$ .

↳ Will not go into details of transmission lines as you have already studied that in EMFT. (2<sup>nd</sup> year).



⇒ Incident wave is shown by sign (+),  $V^+(x)$ .

⇒ Reflected wave is shown by sign (-)  $V^-(x)$ .

$$\Rightarrow \underset{\substack{\uparrow \\ \text{Incident} \\ \text{Wave}}}{V^+(x)} = \underset{\substack{\uparrow \\ \text{Constant}}}{C_1} e^{-j\beta x}$$

This term comes here because  $x=0$  here.

⇒ Similarly for reflected wave,  $V^-(x) = C_2 e^{+j\beta x}$  (Have sign because it is)

Note:-  
=

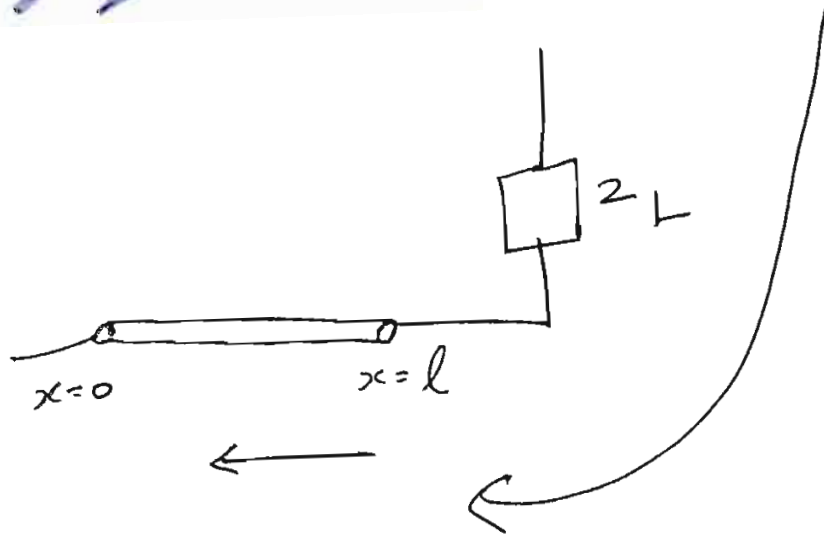
~~equation~~  
$$V^-(x) = C_2 e^{j\beta x}$$

The (+)ve sign here does not

mean that it is going to be (+)ve. Look at the

fig. of transmission line. 'x' is going to be (-)ve

when you are going from  $x=l$  to  $x=0$ .



⇒ Total voltage,

$$\left[ \begin{array}{ccc} V(x) = & V^+(x) + & V^-(x) \\ \uparrow & \uparrow & \uparrow \\ \text{Total} & \text{Incident} & \text{Reflected} \\ \text{voltage} & \text{voltage} & \text{voltage} \end{array} \right]$$

⊥ (L) Note:- This is same as we have talked earlier about  $V_1$  for port-1.

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⇒ Similarly,

$$\begin{aligned} \text{Total current, } I(x) &= I^+(x) + I^-(x) \\ &= \frac{V^+(x)}{Z_0} - \frac{V^-(x)}{Z_0} \end{aligned}$$

⇒ At any port of the network,

$$a = \frac{V^+}{\sqrt{Z_0}}, \quad b = \frac{V^-}{\sqrt{Z_0}}$$

⇒ If you forgot what is 'a' & 'b' then check previous lectures.

↳ This is generalized one

ex:- If it is port '1' then we will write

$$a_1 = \frac{V_1^+}{\sqrt{Z_0}}, \quad b_1 = \frac{V_1^-}{\sqrt{Z_0}}$$

similarly for port '2' it will be,

$$a_2 = \frac{V_2^+}{\sqrt{Z_0}}, \quad b_2 = \frac{V_2^-}{\sqrt{Z_0}}$$

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⇒ Reflection coefficient ( $\Gamma$ ) =  $\frac{\text{Reflected Power}}{\text{Incident}}$

↳  $S_{11}, S_{22}, S_{33}$  etc

↓  
Depending upon  
which port we  
are looking at.

$$\therefore \left[ \Gamma = \frac{V^-}{V^+} = \frac{b \sqrt{Z_0}}{a \sqrt{Z_0}} = \frac{b}{a} \right]$$

⇒ So, reflection coefficient at Port-1 will be

$$\Gamma_1 = \frac{b_1}{a_1}$$

Similarly  $\Gamma$  at Port 2  $\Gamma_2 = \frac{b_2}{a_2}$ , and so on.

ABCD to S-Parameter  $\Leftarrow$  No need of derivation.

S	ABCD
$S_{11}$	$\frac{A + (B/Z_0) - CZ_0 - D}{A + (B/Z_0) + CZ_0 + D}$
$S_{12}$	$\frac{2(CA - BD)}{A + (B/Z_0) + CZ_0 + D}$
$S_{21}$	$\frac{2}{A + (B/Z_0) + CZ_0 + D}$
$S_{22}$	$\frac{-A + B/Z_0 - CZ_0 + D}{A + (B/Z_0) + CZ_0 + D}$

For symmetrical Network  
 $S_{11} = S_{22}$   
 $(A = D)$   
 For reciprocal network  
 $S_{21} = S_{12}$   
 $(AD - BC = 1)$

(refer Pozar book if you are interested!)

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Note:- ① We are ~~doing~~ doing this conversion because  
 = We know how a large network can be divided into smaller network for which we use ABCD Parameters (Previous lecture).

↳ We multiplied ABCD matrix of individual networks, for finding overall ABCD matrix.

② Our objective is not ABCD when we are talking about MLave. In microwave we talk about incident wave & reflected wave. So, we are more interested in finding S-Parameters.

③ So, the ABCD Parameters that we discussed in previous lectures is an intermediate step to reach the final goal of S-Parameters.

Note:-

Now,

$$S_{11} = \frac{A + (B/Z_0) - CZ_0 - D}{A + (B/Z_0) + CZ_0 + D}$$

What is unit of 'A' → It is dimensionless

" 'D' → Dimensionless

" 'B' → unit of impedance

So,  $B/Z_0$  → Dimensionless.

Unit of 'C' =  $mho$

So,  $CZ_0 \rightarrow$  Dimensionless

$$\Rightarrow \text{So, } \frac{A + B/Z_0 - CZ_0 - D}{A + B/Z_0 + CZ_0 + D}$$

can be written in ~~the~~ the form of normalized values.

$$\text{Let } S_{11} = \frac{a + b - c - d}{a + b + c + d}$$

Let normalized value be,

$$A = a, \quad \frac{B}{Z_0} = b, \quad CZ_0 = c, \quad D = d$$

$$\therefore \left[ S_{11} = \frac{a + b - c - d}{a + b + c + d} \right]$$

Note:- In all parameters ( $S_{11}, S_{12}, S_{21}, S_{22}$ )

mentioned in table denominators are same,

i.e.  $A + B/Z_0 + CZ_0 + D$ .

Now look at numerator,

$$S_{11} = \frac{A + B/Z_0 - CZ_0 - D}{A + B/Z_0 + CZ_0 + A}$$

← Numerator

$$S_{22} = \frac{-A + B/Z_0 - CZ_0 + D}{A + B/Z_0 + CZ_0 + A}$$

← Numerator

i.e. in Normalized form numerator will be,

$$S_{11} = a + b - c - d$$

$$S_{22} = -a + b - c + d$$

←

In these two equations 'a' has become '-a'

& '-d' has become 'd'.

Otherwise  $S_{11}$  &  $S_{22}$  are exactly same.

⇒ Using Symmetrical Property,

$$\text{if } [A = D]$$

Then,

$$S_{11} = \frac{\cancel{A} + B/Z_0 - CZ_0 - \cancel{A}}{\cancel{A} + B/Z_0 + CZ_0 + \cancel{A}} = \frac{B/Z_0 - CZ_0}{B/Z_0 + CZ_0 + A}$$

$$S_{22} = \frac{-\cancel{A} + B/Z_0 - CZ_0 + \cancel{A}}{A + B/Z_0 + CZ_0 + A} = \frac{B/Z_0 - CZ_0}{B/Z_0 + CZ_0 + A}$$

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$$\therefore [S_{11} = S_{22}]$$

↳ So, we can easily prove from  $S_{11} = S_{22}$  or  $A = D$  that it is symmetrical network.

Note:- Now let's look at  $S_{12}$  &  $S_{21}$ .

Numerator is,

$$S_{12} = 2(AD - BC)$$

$$S_{21} = 2$$

For reciprocal network,  $AD - BC = 1$   $\Rightarrow$   $\therefore S_{12} = \frac{2}{A + B/Z_0 + CZ_0 + D}$   
 &  $S_{21} = \frac{2}{A + \frac{B}{Z_0} + CZ_0 + D}$

$$\therefore [S_{12} = S_{21}]$$

Note:- In some books they have shown how to convert from S-Parameter to ABCD. But in MLave we don't need this.

We need only ABCD to S-parameter conversion.



Note:-

We know,

$$I(x) = I^+(x) + I^-(x)$$

$\Rightarrow$

$$= \frac{V^+(x)}{Z_0} - \frac{V^-(x)}{Z_0}$$

$$\Rightarrow a = \frac{V^+}{\sqrt{Z_0}} \quad \text{i.e.} \quad V^+ = a\sqrt{Z_0}$$

$$b = \frac{V^-}{\sqrt{Z_0}} \quad \text{i.e.} \quad V^- = b\sqrt{Z_0}$$

$$\therefore I(x) = I^+(x) + I^-(x) \quad \left\{ \begin{array}{l} \text{both are} \\ \text{same.} \end{array} \right.$$

$$I = I^+ + I^- \quad \left\{ \begin{array}{l} \text{If you don't} \\ \text{want to} \\ \text{write 'x'} \end{array} \right.$$

$$= \frac{a\sqrt{Z_0}}{Z_0} - \frac{b\sqrt{Z_0}}{Z_0}$$