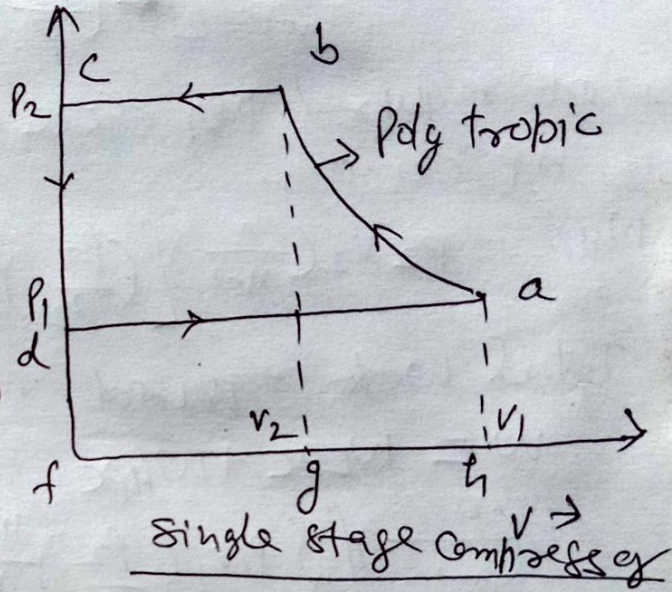


Topic - Compressor →

work Required in single stage Compressor without clearance volume →

The initial conditions of air are,  
 pressure =  $P_1$  (bar)  
 volume =  $V_1$  ( $m^3$ )  
 and is compressed to final condition of pressure -  $P_2$  (bar)  
 and volume =  $V_2$  ( $m^3$ )



work required per cycle,

$$W = \text{Area } abcd = \text{Area } cbgf + \text{Area } gbah - \text{Area } adfh$$

$$W = P_2 V_2 + \frac{P_2 V_2 - P_1 V_1}{\eta - 1} - P_1 V_1$$

$$= \frac{P_2 V_2 (\eta - 1) - P_1 V_1 (\eta - 1) + P_2 V_2 - P_1 V_1}{\eta - 1}$$

$$W = \frac{\eta P_2 V_2 - P_2 V_2 - \eta P_1 V_1 + P_1 V_1 + P_2 V_2 - P_1 V_1}{\eta - 1}$$

$$W = \frac{\eta}{\eta - 1} (P_2 V_2 - P_1 V_1) = P_1 V_1 \left( \frac{\eta}{\eta - 1} \right) \left( \frac{P_2 V_2}{P_1 V_1} - 1 \right)$$

for polytropic compression

$$P_1 V_1^\eta = P_2 V_2^\eta \Rightarrow \frac{V_2}{V_1} = \left( \frac{P_2}{P_1} \right)^{\frac{1}{\eta}}$$

$$\therefore W = P_1 V_1 \left( \frac{\eta}{\eta - 1} \right) \left[ \frac{P_2}{P_1} \left( \frac{P_2}{P_1} \right)^{\frac{1}{\eta} - 1} - 1 \right]$$

$$W = P_1 V_1 \left( \frac{\eta}{\eta - 1} \right) \left[ \left( \frac{P_2}{P_1} \right)^{\frac{\eta}{\eta - 1}} - 1 \right]$$

$$W = \frac{\eta}{\eta - 1} m R T \left[ \left( \frac{P_2}{P_1} \right)^{\frac{\eta}{\eta - 1}} - 1 \right] \quad \left[ \because P_1 V_1 = m R T \right]$$

Discharge temp of air,  $T_2 = T_1 \left( \frac{P_2}{P_1} \right)^{\frac{\eta}{\eta - 1}}$



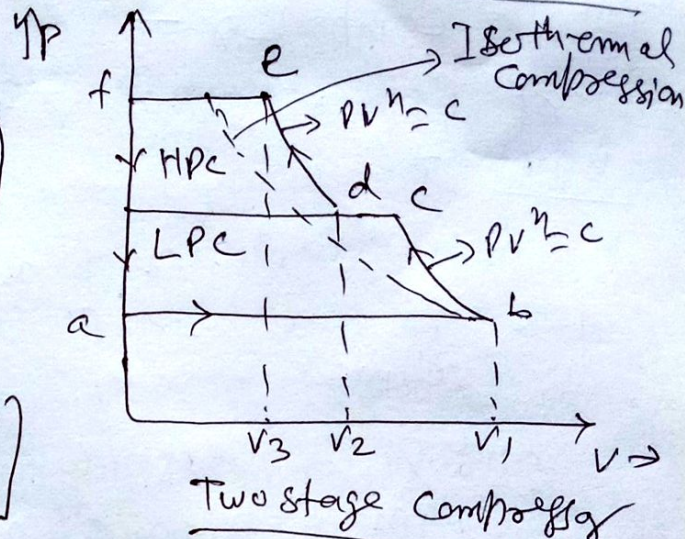
Work Required in two stage compressors without clearance Pg-2

Work required per cycle in L.P. cylinder -

$$W_{LPC} = p_1 v_1 \left( \frac{\gamma}{\gamma-1} \right) \left[ \left( \frac{p_2}{p_1} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]$$

Work required per cycle in HP cylinder.

$$W_{HPC} = p_2 v_2 \left( \frac{\gamma}{\gamma-1} \right) \left[ \left( \frac{p_3}{p_2} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]$$



Total work required

$$W = W_{LPC} + W_{HPC}$$

$$= \left( \frac{\gamma}{\gamma-1} \right) \left[ p_1 v_1 \left( \frac{p_2}{p_1} \right)^{\frac{\gamma-1}{\gamma}} + p_2 v_2 \left( \frac{p_3}{p_2} \right)^{\frac{\gamma-1}{\gamma}} - 2 \right]$$

if intercooling is perfect

$$p_1 v_1 = p_2 v_2$$

$$W = p_1 v_1 \left( \frac{\gamma}{\gamma-1} \right) \left[ \left( \frac{p_2}{p_1} \right)^{\frac{\gamma-1}{\gamma}} + \left( \frac{p_3}{p_2} \right)^{\frac{\gamma-1}{\gamma}} - 2 \right]$$

$$p_1 v_1 = m R T_1 = m R T_a$$

$$m = \frac{p_1 v_1}{R T_a}$$

$$p_1 v_1^\gamma = p_2 v_c^\gamma$$

$$p_2 v_c = m R T_c$$

$$T_c = \frac{p_2 v_c}{m R}$$

Substituting the value of m and v\_c to

calculate T\_c

$$\frac{p_2 v_c}{T_c} = \frac{p_2 v_2}{T_d}$$

$$T_d = \frac{p_2 v_2}{p_2 v_c} \times T_c$$

$$= \frac{v_2}{v_c} \times T_c$$

Calculate the value of T\_d  
Heat Rejected in the intercooler -

$$Q_{ic} = m C_p (T_c - T_d)$$